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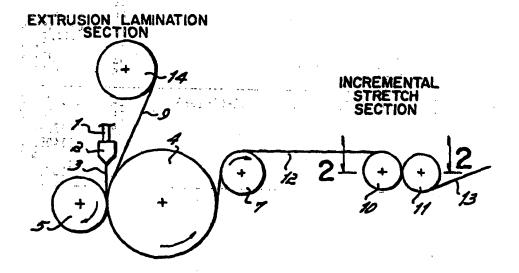
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(54) Title: METHOD OF MAKING A CLOTH-LIKE MICROPOROUS LAMINATE OF A NONWOVEN FIBROUS WEB AND THERMOPLASTIC FILM



#### (57) Abstract

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A cloth-like microporous laminate of a nonwoven fibrous web and thermoplastic film is made by lamination of a microporous-formable film composition and a nonwoven fibrous web followed by incremental stretching to form the cloth-like microporous laminate. The cloth-like microporous laminate has air and moisture vapor permeabilities, but acts as a barrier to the passage of liquids. The cloth-like laminates are especially useful in fabricating garments in order to provide the breathable qualities of air and moisture vapor transmission with liquid-barrier properties. Such garments include baby diapers, baby training pants, catamenial pads and garments, and the like where moisture vapor and air transmission-properties, as well as fluid barrier properties, are needed.

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METHOD OF MAKING A CLOTH-LIKE MICROPOROUS LAMINATE OF A NONWOVEN FIBROUS WEB AND THERMOPLASTIC FILM

#### **BACKGROUND OF THE INVENTION**

Processes of bonding nonwoven fibrous webs to thermoplastic films have been known for some time. Additionally, methods for extrusion laminating thermoplastic films to unstretched nonwoven webs are well-known in the art.

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Relevant patents regarding extrusion lamination of unstretched nonwoven webs include U. S. Patent Nos. 2,714,571; 3,058,868; 4,522,203; 4,614,679; 4,692,368; 4,753,840 and 5,035,941. The above '863 and '368 patents disclose stretching extruded polymeric films prior to laminating with unstretched nonwoven fibrous webs at pressure roller nips. The '203 and '941 patents are directed to co-extruding multiple polymeric films with unstretched nonwoven webs at pressure roller nips. The '840 pat nt discloses preforming nonwoven polymeric fiber materials pri r t extrusion laminating with films to improve bonding between the nonwoven fibers and films. More specifically, the '840 patent

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discloses conventional embossing techniques to form densified and undensified areas in nonwoven bas plies prior to extrusion lamination to improve bonding between nonwoven fibrous webs and films by means of the densified fiber areas. The '941 patent also teaches that unstretched nonwoven webs that are extrusion laminated to single ply polymeric films are susceptible to pinholes caused by fibers extending generally vertically from the plane of the fiber substrate and, accordingly, this patent discloses using multiple co-extruded film plies to prevent pinhole problems. Furthermore, methods for bonding loose nonwoven fibers to polymeric film are disclosed in U. S. Patent Nos. 3,622,422; 4,379,197 and 4,725,473.

It has also been known to stretch nonwoven fibrous w bs using intermeshing rollers to reduce basis weight and examples of patents in this area are U. S. Patent Nos. 4,153,664 and 4,517,714. The '664 patent discloses a method of incremental cross direction (CD) or machine direction (MD) stretching nonwoven fibrous webs using a pair of interdigitating rollers to strengthen and soften nonwoven webs. The '664 patent also discloses an alternative embodiment wherein the nonwoven fibrous web is laminated to the thermoplastic film prior to intermesh stretching.

Efforts have also been made to make breathable n n-woven composite barrier fabrics which are impervious to liquids, but which are permeable to water vapor. United States Patent No. 5,409,761 is an example of a fabrication process from the patent art. According to this '761 patent, a nonwoven composite fabric is made by ultrasonically bonding a microporous thermoplastic film to a layer of nonwoven fibro. thermoplastic material. These methods and other methods of making breathable laminates of nonwoven and thermoplastic materials tend to involve expensive manufacturing techniques and/or expensive raw materials.

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The is-a continuing need for improved breathable laminates f nonwoven fibrous substrates and thermoplastic films that provide air and moisture vapor permeabilities with liquid-barrier properties. It would be very desirable to further improve methods of rnaking such breathable laminates and to expand their utiliti s in articles of clothing and other useful products. Improvements are also desirable in methods of producing laminates on high-speed production machinery.

#### SUMMARY OF THE INVENTION.

This invention is directed to a method of making a cloth-like microporous laminate of a nonwoven fibrous web and thermoplastic film. The microporous laminate has air and moisture vapor permeabilities, but acts as a liquid barrier. The laminate is als cloth-like by providing a nonwoven fibrous soft fabric feel. Thus, breathable laminates of this invention are especially useful in the field of garments where breathable and barrier properties are important, f r instance, in medical garments where it is desired to prevent the passage of body fluids or blood to or from the worker while allowing the passage of moisture vapor, It is also desirable to provide garm into which are gas or air permeable to provide enhanced comfort f r the wearer by allowing the perspiration to escape while maintaining a barrier to the passage of liquids.

The method of this invention involves lamination by extrusion or adhesion of the nonwoven fibrous web to a microporousformable thermoplastic film. The microporous-formable thermoplastic composition of the film laminate may comprise a blend of a thermoplastic polymer and a mechanical pore-forming agent such as an inorganic filler. The pore-forming agent in the film laminate is then The state of the section of the sect of the fibrous web and film. This unique method provides economies in manufacturing breathable laminates. However, other microporous-

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formable compositions may be used in the process as further described h reinafter.

In the most preferred form, the method of this invention is conducted on high-speed production machinery on the ord r of about 200-500 fpm. More specifically, a nonwoven fibrous web is introduced into a nip of rollers for extrusion lamination with a microporous-formable thermoplastic film or extrudate. A thermoplastic extrudate is extruded into the nip at a temperature above its softening point to form a film laminated to the fibrous web. The compressiv force between the fibrous web and extrudate is controlled to bond one surface of the web to the film to form a laminate. As indicated above, the laminate may also be formed by adhesively bonding the fibr us web to the microporous-formable film. The thus formed laminate is then incrementally stretched along lines substantially uniformly across the laminate and throughout its depth to render the film microporous. By applying an incremental stretching force to the laminate, both th web and the film are stretched. Incrementally stretching the film at ambient or room temperature where the microporous-formable thermoplastic composition contains a mechanical pore-forming filler such as calcium carbonate, causes microporosity to develop in the film whereby the film is capable of transmitting moisture vapor and air, but acts as a parrier to the transmission of liquid. Breathable cloth-like liquid barriers are economically provided by this invention.

Other benefits, advantages and objectives of this invention will be further understood with reference to the following detailed description.

#### **DETAILED DESCRIPTION**

It is a primary objective of this invention to produce a breathable or microporous laminated sheet of a nonwoven fibrous web and a micropor us therm plastic film on high-speed pr duction machinery. It is the further objective of this invention to produc such

laminates having satisfactory bond str ngths while maintaining the appearance of a fabric or cloth having suitable moisture vapor transmission rates and air permeability, while maintaining liquid-barrier properties. As developed above, these and other objectives are achieved in a preferred form of the invention by first laminating a nonwoven fibrous web and a microporous-formable thermoplastic film. Then, it has been found, by incrementally stretching the laminate, that Bibreathable or microporous laminate is produced where the fibr us web is bonded to the microporous film. The microporous film is characterized by being impervious to the passage of liquid by virtue of the thermoplastic film while maintaining a soft feel on the fibrous web surface of the laminate. Various degrees of moisture vapor or air permeabilities may be achieved in the laminate by providing th microporos in the range of about 0.1 micron to about 1 micron. The 15 description and the second compares the provided by employing microporous-formable thermoplastic compositions which include a pore-forming filler such as calcium carbonate, diatomaceous earth, or titanium dioxide, or combinations thereof having an average particle size of about 0.5 to about 5 microns. The pore-forming filler in the extruded film is activated by mechanical incremental stretching of the film. In an alternative form, a microporous-formable thermoplastic composition may be obtained by blending different polymers which, when and the second as incrementally stretched, provide microporosity as described in U.S. The Street of the Age of Patent Nos. 5,200,247 and 5,407,979 which are incorporated herein 27 by reference. A service of the se

Thus, the method of this invention provides a micropor us laminate having the desired cloth-like features to achieve utility in a number of applications including diapers, pants, surgical gowns, sheets, dressings, hygienic products, and the like. Garments of these types are made very comfortable by the use of these laminates in view 

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#### A. Materials for the Laminate

The microporous-formable film composition can beachieved by formulating a thermoplastic polymer with suitable additives and pore-forming fillers to provide an extrudate or film for Microporous-formable lamination with the nonwoven web. compositions of polyolefins, inorganic pore-forming fillers and other additives to make microporous sheet materials are known. However, it has not been known to laminate such compositions with a nonwov n fibrous web and then incrementally stretch the laminate to create microporosity in the laminate. This method may be done inline and provides economies in manufacturing and/or materials over known methods of making laminates. In addition, as developed above, microporous-formable polymer compositions may be obtained from blends of polymers such as a blend of an alkanovi polymer and polyvinyl alcohol as described in U. S. Patent No. 5,200,247. In addition, blends of an alkanovi polymer, destructured starch and an ethylene copolymer may be used as the microporous-formable polymer composition as described in U.S. Patent No. 5,407,979. With these polymer blends, it is unnecessary to use pore-forming fillers to provide microporosity upon incremental stretching. Rather, the different polymer phases in the film themselves, when the film is stretched at ambient or room temperature, produce microvoids.

The microporous-formable thermoplastic film preferably is of the polyolefin type and may be any of the class of thermoplastic polyolefin polymers that are processible into a film for direct lamination by melt extrusion onto the fibrous web. A number of thermoplastic polymers suitable in the practice of the invention are of the normally-solid oxyalkanoyl polymers or dialkanoyl polymers represented by poly(caprolactone) blended with polyvinylalcohol or starch polymers that may be film-formed. The olefin bas d polymers include the most common ethylene or propylene based polymers such as polyethyl ne,

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polypropylene, and copolymers such as ethylene vinylacetate (EVA). ethylene methyl acrylate (EMA) and ethyl ne acrylic acid (EAA), or the state of such polyolefins. Other examples of polymers suitable for use as films in the composite sheet of this invention are known with reference to the above identified patents cited in the background of this invention and these are incorporated herein by reference.

The nonwoven fibrous web may comprise fib rs of polyethylene, polypropylene, polyesters, rayon, cellulose, nylon, and blends of such fibers. A number of definitions have been proposed for and the state of t As used herein "nonwoven fibrous web" is us d the process of the second second to the second seco relatively flat, flexible and porous, and is composed of staple fibers or continuous filaments.. For a detailed description of nonwovens, se 15 Nonwoven Fabric Primer and Reference Sampler" by E. A. Vaughn, Association of the Nonwoven Fabrics Industry, 3d Edition (1992).

In a preferred form, the microporous laminate employs a film having a gauge or a thickness between about 0.25 and 10 mils and, depending upon use, the film thickness will vary and, most preferably, in disposable applications is the order of about 0.25 to 2 mils in thickness. The ponyoven fibrous webs of the laminated sheet normally have a weight of about 5 grams per square yard to 75 grams per square yard preferably about 20 to about 40 grams per square yard. When employing adhesive lamination, adhesives such as h t melt adhesive, water base adhesive or solid base adhesive may be used. The composite or laminate can be incrementally stretched in the cross direction (CD) to form a CD stretched composite. Furthermore, CD stretching may be followed by stretching in the machine direction (MD) to form a composite which is stretched in both CD and MD directions. As indicated above, the microporous composite or laminate may be used in many different applications such as baby diap is, baby

training pants, catamenial pads and garments, and the like where moisture vapor and air transmission properties, as well as fluid barrier properties, are needed.

#### B. Stretchers for the Microporous-Formable Laminates

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A number of different stretchers and techniques may be employed to stretch the starting or original laminate of a nonwoven fibrous web and microporous-formable film. These laminates of nonwoven carded fibrous webs of staple fibers or nonwoven spunbonded fibrous webs may be stretched with the stretchers and techniques described as follows:

1. Diagonal Intermeshing Stretcher

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The diagonal intermeshing stretcher consists of a pair f left hand and right hand helical gear-like elements on parallel shafts. The shafts are disposed between two machine side plates, the lower shaft being located in fixed bearings and the upper shaft being located in bearings in vertically slidable members. The slidable members ar adjustable in the vertical direction by wedge shaped elements operable by adjusting screws. Screwing the wedges out or in will move the vertically slidable member respectively down or up to further engag or disengage the gear-like teeth of the upper intermeshing roll with the lower intermeshing roll. Micrometers mounted to the side frames are operable to indicate the depth of engagement of the teeth of the intermeshing roll.

Air cylinders are employed to hold the slidable members in their lower engaged position firmly against the adjusting wedges to oppose the upward force exerted by the material being stretched. These cylinders may also be retracted to disengage the upper and lower intermeshing rolls from each other for purposes of threading material through the intermeshing equipment or in conjunction with a safety circuit which would op n all the machine nip p ints when activated.

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A drive means is typically utilized to drive the stationery intermeshing roll. If the upper intermeshing roll is to be disengageable for purposes of machine threading or safety, it is preferable to use an antibacklash gearing arrangement between the upper and lower intermeshing rolls to assure that upon reengagement the teeth of one intermeshing roll always fall between the teeth of the other intermeshing roll and potentially damaging physical contact between addenda of intermeshing teeth is avoided. If the intermeshing rolls are to remain in-constant engagement, the upper intermeshing roll typically need not be driven. Drive may be accomplished by the driven intermeshing roll through the material being stretched.

The intermeshing rolls closely resemble fine pitch helical gears. In the preferred embodiment, the rolls have 5.935" diameter, 45° helix angle, a 0.100" normal pitch, 30 diametral pitch, 14½° 15 pressure angle, and are basically a long addendum topped gear. This produces a narrow, deep tooth profile which allows up to about 0.090 of intermeshing engagement and about 0.005 clearanc on the sides of the tooth for material thickness. The teeth are not designed to transmit rotational torque and do not contact metal-to-20 metal in normal interreshing stretching operation.

## 2. Cross Direction Intermeshing Stretcher

The CD intermeshing stretching equipment is identical to the diagonal intermeshing stretcher with differences in the design of and the minor areas noted below. Since the 25 CD intermeshing elements are capable of large engagement depths, it is important that the equipment incorporate a means of causing th shafts of the two intermeshing rolls to remain parallel when the top shaft is raising or lowering. This is necessary to assure that the t eth of one intermeshing roll always fall between the teeth of the other intermeshing roll and potentially damaging physical contact between interm shing teeth is avoided. This parallel motion is assured by a

rack and gear arrangement wherein a stationary gear rack is attached to each side frame in juxtaposition to the vertically slidable members. A shaft traverses the side frames and operates in a bearing in each of the vertically slidable members. A gear resides on each end of this shaft and operates in engagement with the racks to produce the desired parallel motion.

The drive for the CD intermeshing stretcher must operate both upper and lower intermeshing rolls except in the cas of intermeshing stretching of materials with a relatively high coefficient of friction. The drive need not be antibacklash, however, because a small amount of machine direction misalignment or drive slippage will cause no problem. The reason for this will become evident with a description of the CD intermeshing elements.

The CD intermeshing elements are machined from s lid material but can best be described as an alternating stack of tw different diameter disks. In the preferred embodiment, the intermeshing disks would be 6" in diameter, 0.031" thick, and have a full radius on their edge. The spacer disks separating the intermeshing disks would be 5 1/2" in diameter and 0.069" in thickness. Two rolls of this configuration would be able to be intermeshed up to 0.231" leaving 0.019" clearance for material on all sides. As with the diagonal intermeshing stretcher, this CD intermeshing element configuration would have a 0.100" pitch.

#### 3. Machine Direction Intermeshing Stretcher

The MD intermeshing stretching equipment is identical to the diagonal intermeshing stretch except for the design of the intermeshing rolls. The MD intermeshing rolls closely resemble fine pitch spur gears. In the preferred embodiment, the rolls have a 5.933" diameter, 0.100" pitch, 30 Diametral pitch, 14½° pressure angle, and are basically a I ng addendum, topped gear. A second pass was taken on these rolls with the gear hob offset 0.010" to provide a narrowed

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tooth with more clarance. With about 0.090" of engagement, this configuration will have about 0.010" clearance on the sides for material thickness.

#### Incremental Stretching Technique

The above described diagonal, CD or MD intermeshing stretchers may be employed to produce the incrementally stretched laminate of nonwoven fibrous web and microporous-formable film to form the microporous laminate of this invention. The stretching operation is usually employed on an extrusion laminate of a nonwoven stable fibers or spun-bonded filaments and States and the state of the unique aspects of this invention a laminate of a nonwoven fibrous web of spunbonded filaments may be incrementally stretched to provide a very soft fibrous finish to the laminate that looks like cloth. The laminate f nonwoven fibrous web and microporous-formable film is incrementally stretched using, for Instance, the CD and/or MD intermeshing stretcher with one pass through the stretcher with a depth of roller engagem int at about 0.060 inch to 0.120 inch at speeds from about 200 fpm to 500 fpm or faster. The results of such incremental or intermesh stretching produces laminates that have excellent breathability and liquid-barrier properties, yet provide superior bond strengths and s ft cloth-like textures

#### DETAILED EXAMPLES OF THE INVENTION

The following examples illustrate the microp r us 25 laminates of this invention and methods of making them. In light of these examples and this further detailed description, it is apparent t a person of ordinary skill in the art that variations thereof may be made without departing from the scope of this invention.

The invention is further understood with reference to the To rain a look of 30 or or drawings in which; and a refer or or or

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Fig. 1 is a schematic of an inline extrusi in laminati in and incremental stretching apparatus for making the micropor us laminate of this invention.

Fig. 2 is a cross sectional view taken along the line 2-2 of Fig. 1 illustrating the intermeshing rollers in diagrammatic form.

Fig. 3 is a graph demonstrating the air permeability properties of cloth-like microporous laminates.

Fig. 4 is a graph demonstrating the moisture vapor transmission properties of microporous laminates for comparison with non-microporous films and/or composites.

#### **EXAMPLE 1.**

A blend of polyethylene and ethylene vinyl acetate having the following composition was extrusion laminated to a nonwoven fibrous web of spun-bonded polyethylene and then incrementally stretched to provide a microporous laminate.

34.1% of polyethylene (Dowlex 2045 from Dow Chemical)

11.4% of ethylene vinyl acetate (Elvax 3128 from DuPont)

45.5% of stearic acid treated calcium carbonate (particle size from about 0.5 to 8 microns with an average of about 1 micron)

#### 9.1% of glycerol monostearate

One spun-bonded polyethylene fibrous web of 28 grams/yd<sup>2</sup> weight was laminated by extrusion of the ab ve microporous-formable composition employing the extrusion laminator of Fig. 1. As shown schematically in Fig. 1, the incoming web 9 from roller 14 was introduced into the nip of a rubber roll 5 and a metal roll 4. The polyethylene extrudate or film 3 from extruder 1 was extruded through die 2 into the nip while the nonwov n fibrous w b 9 was introduced. Typically, at speeds over 300 fpm in this extrusion

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lamination section, the polyethylene film 3 on the order of ab ut 0.25 to 10 mils in thickness is laminated at melt temperatures on the order of about 400-500° F to form the laminate 12 which is taken off at roller 7. The compressive force at the nip is controlled such that the webs are bonded to the polyolefin film to avoid pinholing and pr s rve the fibrous feel on the fiber surfaces of the laminate 12. Pressures in the order of about 10 to 80 psi are sufficient to achieve satisfactory bond for fibrous webs of about 5 to 75 grams/yd2. The laminate produced by the extrusion of Fig. 1 does not show any air flow (see Fig. 3, Curve 2).

While the pressure at the nip of rolls 4,5 is us d t laminate the web and film 3, it should be understood that a vacuum roller can also be used at the nip to cause lamination.

As shown schematically in Fig. 1, where the inc ming laminate 12 at an ambient temperature of about 70-90° F was passed through the CD incremental stretcher rollers 10 and 11 at a depth of roller engagement of about 0.100" at about 300 fpm, a micropor us laminate 13 of this invention was formed. The intermeshing rollers 10 and 11, which are diagrammatically shown in Fig. 2 have been described above to illustrate the uniform stretching along lines across the laminate (CD) in a first direction and through the depth of the laminate. The MD stretcher rollers which have been described above, but are not shown in Fig. 1, stretch the laminate at a depth of negative to the engagement of about 0.060" at about 300 fpm in a second direction substantially perpendicular to the first directional stretch. Under these stretching conditions, the calcium carbonate in the polymer formulati n aids in forming a microporous laminate. The microporous laminate 13, after CD and MD stretching, does show air flow (see Fig. 3, Curve 1) ううない カランでは Subject equit equit equit moisture vapor transmission rate (see Fig. 4, Curve 1).

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#### Example 2.

The microporous-formable composition of Example 1 was extrusion laminated in a manner similar to that of Example 1 and the bond strength was controlled to result in a tight bond, but peelable at a peel force of about 100-500 grams/inch. The microporous-formable laminate was then CD and MD stretched at about 70-90° F at 300 fpm by using the same CD and MD rollers described above at various engagement depths. Table II hereinafter presents the data as a result of these operations and the properties of the resulting micropor us laminate.

TABLE II

11 II-A II-B II-C CD Engagement (inches) 0 0.080 0.100 0.120 MD Engagement (inches) 0.060 0.060 0.060 Total weight of the laminate 64 42 35 30 (grams/yd²) MVTR g/m²/day (ASTM E96E) 15 1140 1500 1700 100° F, 90% RH Air Flow (CC/cm<sup>2</sup>/min) at. 0 2 3 4 5 psig 0 4 10 psig 10 13 20 psig 0 10 20 25 Weight Reduction 0 34 45 52 After Stretching (%)

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#### Example 3.

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The formulation of Example 1 is extruded into a 1.5 mil film gauge and laminated to a spun-bonded polyethylene at 0.8 oz/yd² by using a hot melt spray unit where the adhesive is styrene-isoprenestyrene block copolymer and r sin est r. This laminat d c mposit is then CD intermeshed and stretch d at about 70-90° F at 300 fpm by

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rollers having an engagement depth of 0.110", foll wed by MD stretching with an engagement depth of 0.050" using the same CD/MD stretcher rollers described above. The resulting microp rous laminate has an MVTR (ASTM E96E) of 1515 grams/m²/day at 100° F and 90° RH.

### Example 4.

The collowing additional microporous-formable thermoplastic compositions may be used in making a microporous laminate of this invention (% by weight).

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#### Composition A

Polyolefin (linear low density polyethylene, high d nsity polyethylene, or polypropylene) (17% - 82%)

Inorganic filler (17% -67%)

Liquid or waxy hydrocarbon polymers such as liquid polybutadiene or hydrogenat d

#### Composition B

High density polyethylene (60%)

Ethylene vinyl acetate (6%)

Diatomaceous earth (18%)

Titanium dioxide (0.3%)

Calcium carbonate (6%)

Composition C

Polyethylene (74% - 50%)

Inorganic Filler (26% - 50%)

Composition D

Ethylene propylene diene monomer or ethylene propyl n

Inorganic filler (40% - 80%)

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Composition E

Polybutene - 1 47.4%

Calcium carbonate 47.4%

Polystyrene

5.0%

Stearic Acid

0.2%

In view of the above detailed description, it will be understood that variations will occur in employing the principles of this invention depending upon materials and conditions as will be understood to those of ordinary skill in the art.

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What is claimed is:

1. A method of making a cloth-like breathable and liquid-barrier laminate of a nonwoven fibrous web and a microporous thermoplastic film comprising

formable thermoplastic film into a nip of rollers,

controlling the compressive force between said web and film at the nip to bond the surface of the web to the film to form a laminated sheet,

applying an incremental stretching force at ambient temperature to said laminated sheet along lines substantially uniformly across the laminated sheet and throughout its depth to provide a cloth-like microporous laminate,

whereby said cloth-like microporous laminate transmits moisture vapor and air, and provides a barrier to the passage of liquid.

- 2. The method of claim 1 wherein said cloth-like laminate is formed by extrusion, vacuum or adhesive lamination.
- 3. The method of claim 1 wherein said fibrous web comprises polyolefin fibers.
- 4. The method of claim 1 wherein said microporousformable film is a polyolefin film.

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- 5. The method of claim 1 wherein said fibers are selected from the group consisting of polypropylene, polyethylene, polyesters, cellulose, rayon, nylon, and blends of two or more of such fibers.
- 6. The method of claim 1 wherein said microporousformable film is selected from the group consisting of polyethylene, polypropylene and copolymers thereof containing a pore-forming filler.
- 7. The method of claim 1 wherein said micropor usformable film is selected from the group consisting of polyvinyl alcoh 1, polycaprolactone, starch polymers and blends thereof.
- 8. The method of claim 1 wherein the fibrous web has a weight from about 5 to about 70 grams/yd² and the microporous film has a film thickness of about 0.25 to about 10 mils.
- 9. The method of claim 1 wherein said web is formed from staple or spun-bonded fibers.

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10. A method of extrusion laminating a cloth-like breathable and liquid-barrier laminate of a nonwoven fibrous w b and a microporous thermoplastic film comprising

introducing a continuous length of nonwoven fibrous web into a nipsof rollers for laminating with a microporous-formable thermoplastic film.

continuously extruding into said nip a microporousformable thermoplastic extrudate at a temperature above its soft ning point to form a film,

controlling the compressive force between said w b and ending the surface of the web to the film at the nip to bond the surface of the web to the film to firm a The Property of the Control of the C

continuously introducing inline said laminated she t int incremental stretching rollers at ambient temperature to incrementally stretch said laminated sheet along lines substantially uniformly across the laminated sheet and throughout its depth to provide a cloth-like microporous laminate,

whereby said cloth-like microporous laminate transmits www. 100 100 100 100 100 100 moisture yapor and air and provides a barrier to the passage of liquid.

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- 11. The method of claim 10 wh rein said fib rs are selected fr m the group consisting of polypropylene, polyethylene, polyesters, cellulose, rayon, nylon, and blends of two or more of such fibers, and said microporous-formable film is selected from the group consisting of polyethylene, polypropylene and copolymers thereof containing a pore-forming filler.
- 12. The method of claim 10 wherein said microporousformable film is selected from the group consisting of polyvinyl alc hol, polycaprolactore, starch polymers and blends thereof.
- 13. The method of claim 10 wherein the fibrous web has a weight from about 5 to about 70 grams/yd<sup>2</sup> and the microp rous film has a film thickness of about 0.25 to about 10 mils.
- 14. The method of claim 10 wherein said incremental stretching rollers comprise a first section and a second section and said laminated sheet is incrementally stretched in a first direction by said first section followed by incremental stretching in a second direction by said second section.
- 15. The method of claim 14 wherein said first and second stretching directions are substantially perpendicular to one another.

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INCREMENTAL STRETCH SECTION

FIG. 1

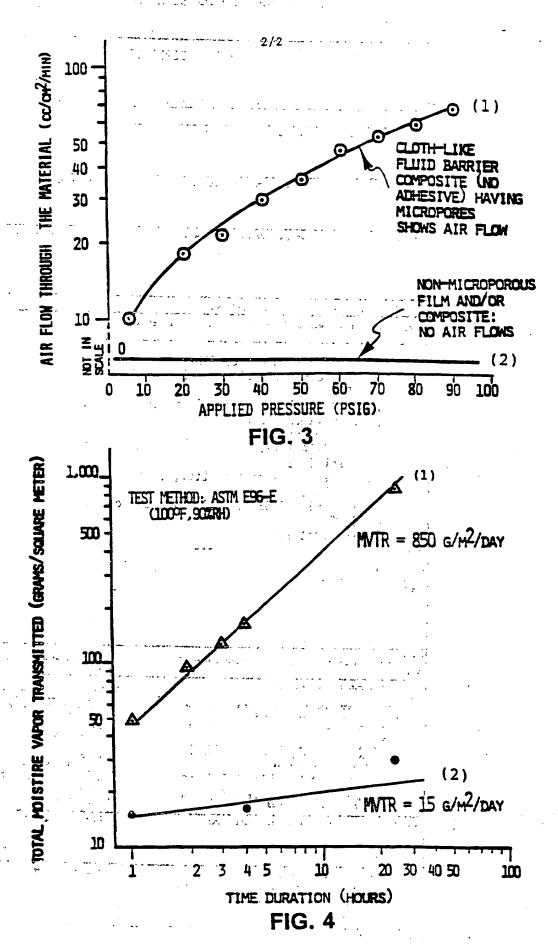
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FIG. 2

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